

Title: Performance Evaluation of Fayda Waste Stabilization Ponds, Duhok, Iraq: Operational Performance, Challenges and Improvement Opportunities

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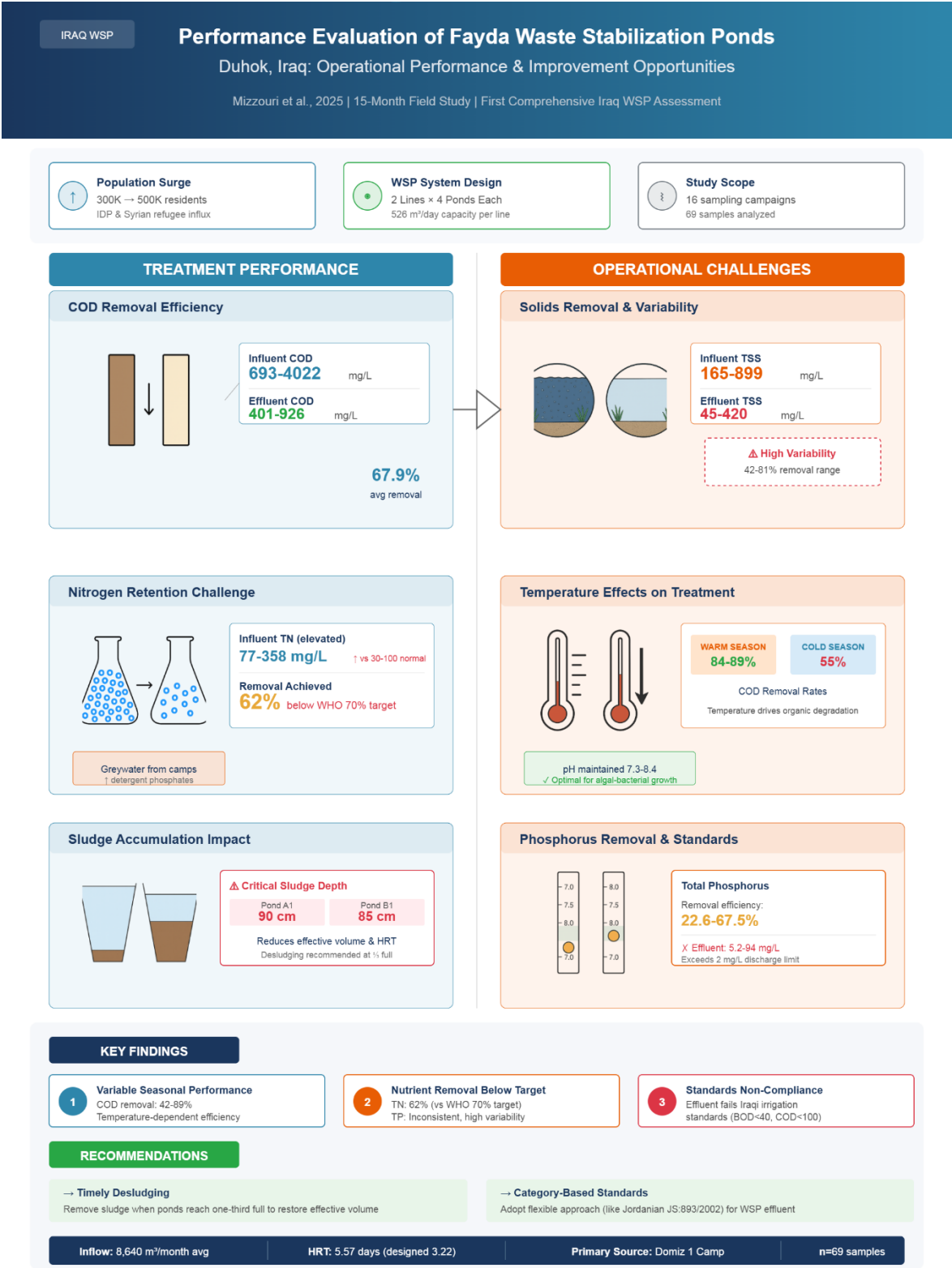
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24 **Abstract:**

25 This study evaluated the operational performance of the Fayda Waste Stabilization Ponds (WSPs) in
26 Duhok, Iraq. Sixteen grab-sampling campaigns were conducted over a 15-month monitoring period,
27 generating 69 wastewater samples from influent sources, pond outlets, and final effluent. Field
28 observations, physicochemical analyses, operational monitoring, and meteorological data were used to
29 assess pollutant removal, identify operational constraints, and evaluate compliance with wastewater
30 reuse standards. Results showed substantial seasonal and operational variability. COD removal ranged
31 from 42.1% to 89.3%, with effluent COD concentrations of 372–926 mg/L. TSS removal ranged from
32 42.31% to 81.08%, while TN removal averaged approximately 65%, remaining below the
33 recommended 70% target. TP removal ranged from 22.6% to 67.5%, indicating inconsistent nutrient
34 removal. Effluent quality frequently failed to meet Iraqi standards for direct discharge or agricultural
35 reuse. Performance limitations were mainly linked to variable influent characteristics, high nutrient
36 loading, graywater inputs, temperature effects, sludge accumulation (90 cm and 85 cm in anaerobic
37 ponds), and improper wastewater disposal. The study recommends influent equalization, controlled
38 loading, regular desludging, improved infrastructure. This study provides the first comprehensive full-
39 scale in situ assessments of WSP performance in Iraq and proposes practical operational measures and
40 a category-based approach for wastewater reuse standards.

41 **Keywords:** Wastewater treatment, nutrient removal, influent characteristics, Iraqi discharge standards,
42 seasonal variations, sludge accumulation, operation and maintenance, pollutant removal efficiency

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47 **1. Introduction**

48 Due to increased water contamination, population growth, and climate changes, there is a deficiency of
49 freshwater resources worldwide (Kan. and Akalin 2025; Mishra 2023). The application of untreated
50 wastewater is widespread in developing countries for irrigation purposes as a result of limited access to
51 clean water thus causing adverse effects on the environment with possible related contaminants (Tariq
52 and Mushtaq; 2023 Heyde et al. 2025).

53 Duhok City has experienced a remarkable increase in population in recent years as a result of increased
54 numbers of internally displaced persons (IDPs) in conflict areas of Iraq and Syrian refugees fleeing
55 Syria, as reported by the United Nations High Commissioner for Refugees (UNHCR 2018). According
56 to the UNHCR (2018), the number of people living in Duhok City increased from about 300,000 in
57 2014 to more than 500,000 in 2018. This rapid population growth has put a lot of stress on local
58 infrastructure, especially the water supply and sewage systems. The International Organization for
59 Migration (IOM 2019) findings also stated that urban areas associated with the Kurdistan area have
60 been severely impacted by displacement in Iraq. The study found that approximately five years after the
61 intensification of conflicts in the region beginning in 2014, Duhok City had a population increase of
62 around 30-40%. This population boom has changed the socio-economic landscape of the city.

63 The majority of countries treat or reuse wastewater before being disposed of into the environment;
64 however, this process can be difficult for developing countries because of high growth rates in their
65 populations, a lack of technical knowledge, and limited awareness regarding wastewater management
66 (Shukri et al. 2024). Therefore, it is essential to develop adequate and cost-effective wastewater
67 treatment technologies that can minimize water contamination while allowing the reuse of wastewater
68 for irrigation, aquaculture, and industrial processes (Krishna et al. 2025; Azoulay et al. 2024).

69 Due to the absence of a wastewater treatment facility, Duhok City's total black wastewater flows
70 directly into each resident's septic tank, where it primarily seeps through the soil until it reaches

71 groundwater (Mizzouri et al. 2020). The high density of unregulated septic systems in Duhok City has
72 proven insufficient and has had a significant impact on public health and regional groundwater quality.
73 Numerous diseases, including diarrhea, cholera, typhoid, and others, can be brought on by bacteria,
74 viruses, protozoa, and fungi present in sanitary wastewater (Mizzouri et al. 2022).

75 A wastewater treatment plant (WWTP) demands highly skilled workers and comes at a very high cost
76 to design and construct. Most of the developing countries are unable to afford the costs. The WSPs are
77 a good alternative to the conventional WWTP since they are a cheap and efficient method to treat both
78 industrial and domestic wastewater. WSP systems have lower capital costs than conventional WWTP,
79 lower technical manpower requirements, easier to design, operate, and maintain, and no reliance on
80 expensive or automated equipment for treatment (Coggins et al. 2018; Pinheiro et al. 2025). These
81 properties make WSP systems interesting. WSP is economical as it relies on natural processes to
82 provide energy demands. It works by using sunlight and microorganisms together (GD and VA 2014;
83 Shaheen et al. 2024). However, WSPs have some disadvantages such as requiring large land areas,
84 effluent quality fluctuation, odor and mosquito problems, and may also emit greenhouse gases (Aydin
85 Uncumusaoğlu 2018; Achag et al. 2023). Moreover, in contrast to other treatment systems, WSPs are
86 influenced by environmental factors such as temperature, rainfall, wind, and evaporation, therefore, they
87 cannot function properly in cold and cloudy regions where biological activity and sunlight for
88 disinfection are limited (Kadri et al. 2021).

89 According to Edokpayi et al. (2017), effluents from WSP systems in most developing countries fail to
90 meet acceptable discharge criteria. A research by Jagals et al. (2006) in South Africa's Free State
91 Province indicated that all 60 WSP systems tested produced effluent that did not meet the
92 recommended standards for fecal indicator organisms. Similarly, Lloyd et al. (2003) emphasized that
93 inadequate operation and maintenance practices of WSPs in Mexico have caused these systems to
94 underperform. The identified operational and maintenance challenges included significant pump

95 malfunctions, untreated sewage bypassing treatment facilities, design flaws, wastewater short-
96 circuiting, and other operational and design issues. Regular desludging of WSPs has been proposed as
97 a valuable intervention technique for performance improvement because, as sludge accumulates, it can
98 decrease effective volume, affect pond hydraulics, and alter treatment performance (Coggins et al.
99 2017). Pond modifications may improve performance. For example, Coggins et al. (2018) stated in
100 their research that baffles installation improved the flow, increased hydraulic retention time (HRT) by
101 20% and reduced wind impacts on pond hydraulics.

102 The Fayda WSPs were constructed in 2020 and have a design capacity of 1052 m³/day. The Fayda
103 WSPs are two lines, each line is a series of four ponds that treat domestic wastewater from Domiz 1
104 camp, Domiz 2 camp, and the city of Duhok and its surroundings. This study differs from previous
105 WSP investigations by providing a full-scale, in situ operational assessment of a pond system serving
106 both refugee camps and host communities under the climatic, hydraulic, and institutional conditions of
107 Duhok Province, rather than relying mainly on laboratory experiments, theoretical models, or
108 conventional municipal case studies. Its scientific contribution lies in linking measured pollutant-
109 removal performance with real operational constraints, including fluctuating influent composition,
110 graywater inputs, sludge accumulation, seasonal loading variation. The hypothesis of this research was
111 to test whether seasonal variations in temperature and influent loading rate have an impact on the
112 removal of pollutants from Fayda WSPs. The objective of this study was to assess whether effluent
113 meets standards and to diagnose performance issues. Moreover, the existing Iraqi requirements for
114 wastewater reuse in irrigation exhibit insufficient flexibility to address the heterogeneity inherent in
115 WSP effluents, depending on a singular effluent parameter that is frequently impracticable. This study
116 directly addresses these gaps by conducting a comprehensive 15-month assessment of the Fayda
117 WSPs. To our knowledge, this is the first such study in Iraq providing empirical data on WSP
118 performance, including influent and effluent parameters, pollutant removal efficiency, and operational

119 efficiency. The innovation of this research is the suggestion of a category-based approach to irrigation
120 reuse, offering a more adaptable framework for wastewater management, acting as a benchmark for
121 other areas in Iraq.

122 **2. Methodology**

123 To address the study objectives, the methodology was organized around four connected components:
124 field characterization of the Fayda WSPs, wastewater sampling and laboratory analysis, operational
125 monitoring, and climatic-data interpretation.

126 **2.1 Description of the study area and site visits**

127 The Fayda WSPs are located in the Sumel District in the Duhok Governorate in the Kurdistan Region
128 of Iraq. It covers about 20,000 m² with geographical coordinates of latitude 36°45'52"N, and longitude
129 42°52'05"E. The plant primarily serves Domiz 1 and Domiz 2 camps in addition to many other areas
130 including Duhok City, Fayda, Domiz, and Sharia sub-districts. The plant consists of two lines of ponds
131 with a total design capacity of 1,052 m³/day. Each line has a design capacity of 526 m³/day. A series of
132 ponds have been constructed on each line (2 anaerobic ponds, 1 facultative pond, and 1 maturation
133 pond). The project also includes an office for the administration, sludge drying beds, and a warehouse
134 for sludge composting (see Figure 1). During the monitoring period, the two treatment lines were
135 operated either simultaneously or individually depending on incoming wastewater volume, organic
136 loading, and operational requirements. Weekly site visits were conducted to Fayda WSP jointly with
137 relevant staff to define the problems of the performance and to monitor the operation of the plant.

138 **2.2 Wastewater Sampling**

139 Over the 13-month study period (May 2021–May 2022), 16 grab samples were collected from the ponds
140 and sources of black wastewater including the camps and local communities. Operational monitoring
141 and field observations were conducted over a 15-month period. A total of 69 wastewater samples were
142 collected from influent sources, pond outlets and final effluent points. All samples were collected

143 between 9:00 and 11:00 AM local time to minimize the diurnal variability of the water quality
144 parameters. Before entering the anaerobic ponds, the raw wastewater (influent) was sampled from the
145 flow splitter chamber. Considering that one outflow served as an inflow for the following pond, samples
146 were subsequently obtained from the outlets of each pond. The final effluent sample was collected from
147 the outlet of the maturation pond. Samples were collected in sterilized glass or polyethylene containers,
148 transported to the laboratory, and stored at 4°C, and analyzed within 24 hours. The raw wastewater-
149 quality data used in the performance assessment are provided in Table S1 as supplementary material.

150 2.3 Monitoring the Performance

151 Operational monitoring focused on the relationship between loading conditions, pond operation,
152 climatic variation, and treatment performance. The organic loading, expressed as biochemical oxygen
153 demand (BOD), was controlled, and different loading patterns were adopted throughout the research
154 period including distributing the load on the ponds' series, operating a series on full loading, or
155 shutting down a series of ponds. In addition, different organic loadings were applied depending on the
156 temperature. For example, organic loading was minimized during snowfall periods to optimize
157 treatment efficacy. The HRT was evaluated by comparing the design flow of 1,052 m³/day with the
158 actual applied flow during the monitoring period. Because the actual applied flow was lower than the
159 design flow, the current HRT values were higher than the original design values. Aerial imagery was
160 acquired during single-series operations to provide information on any potential short-circuiting in the
161 facultative ponds (Figure 1).



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164 **Figure 1.** Annotated aerial view of the Fayda WSPs.

165 2.4 Methods of Analysis

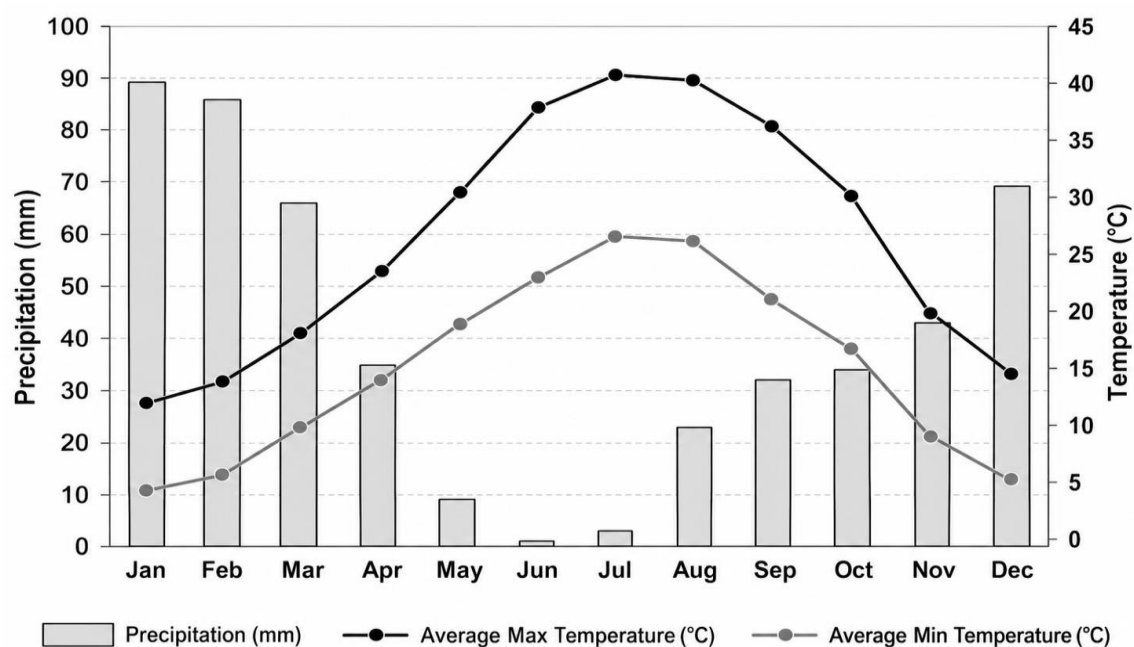
166 The sampling design was therefore intended to capture both source-water variability and treatment
167 progression through the pond sequence, allowing influent quality, intermediate treatment performance,
168 and final effluent quality to be compared. Physicochemical parameters were measured at the site. A
169 HANNA instrument (model HI98199 multi-probe) was used to measure pH, temperature, conductivity,
170 and dissolved oxygen.

171 The samples of wastewater were collected over a span of one year from the sources, influents and
172 effluents of the different ponds of the Fayda WSPs. These samples were stored at 4°C and were
173 eventually analyzed at the Directorate of Environment. The wastewater samples were analyzed for
174 various parameters, namely BOD₅, COD, TSS, TN, TP, pH, and temperature. The parameter analyses
175 were done according to Standard Methods for the Examination of Water and Wastewater (Rice et al.
176 2012). COD determination of wastewater was performed by using procedure 5220 C, standard closed

177 reflux, and titrimetric methods. BOD using method 5210 B, TSS using method 2540 D, TP using
178 method 4500-P E, and TN using method 4500-Norg B (Rice et al. 2012). A limitation of the current
179 assessment is the absence of microbiological data (such as fecal coliforms or helminth eggs). Due to the
180 limitations in laboratory capacity during the study period, the analysis was restricted to physicochemical
181 parameters. Therefore, the present assessment should be interpreted as a physicochemical evaluation of
182 WSP performance rather than a complete sanitary-risk assessment. Microbiological indicators,
183 including fecal coliforms, *E. coli*, intestinal helminth eggs, and other pathogen-related indicators, were
184 not measured and therefore could not be used to assess the public-health safety of the treated effluent.

185 2.5 Meteorological data

186 The Fayda WSPs are working in the climatic conditions of Duhok governorate, where seasonal
187 variation of temperature, precipitation and solar radiation affect the treatment performance. Heavy
188 rainfalls characterize the climate of northern Iraq, particularly Iraqi Kurdistan, which is influenced by
189 the mountain regions inducing the orographic heaving effect (Eklund and Seaquist 2015). The average
190 annual precipitation in the Duhok Governorate is 530 mm based on statistics for the last 10 years
191 (Figure 2). The rainy season usually extends from November to March, and little or no precipitation
192 falls during the summer (June to September). (Eklund and Seaquist 2015). These climatic factors were
193 taken into account in the interpretation of treatment performance since the lower winter temperatures
194 could have reduced microbial activity and conditions in summer could have increased biological
195 degradation and algal activity. Snowfall and snowmelt events were also operationally important as they
196 can temporarily increase hydraulic loading and dilute wastewater entering the ponds.



198

199 **Figure 2:** Climate data based on averages of the two stations in Duhok Governorate covering the period
 200 1998-2014 (Eklund and Seaquist 2015).

201 2.6 Statistical analysis

202 The wastewater-quality dataset was processed using descriptive and inferential statistical analyses. For
 203 each monitored parameter, including COD, TSS, TN, and TP, the mean, standard deviation, minimum,
 204 maximum, and coefficient of variation were calculated for effluent samples where data were available.

205 3 Results and Discussion

206 The results are presented in a sequence that follows the operational pathway of the system: influent
207 quantity, influent and effluent quality, pollutant-removal performance, operational constraints, and
208 practical improvement measures.

209 3.1 Quantity of influent

210 Generally, the majority of the quantities originate from Domiz 1 camp. The quantity in Domiz 1 camp
211 is predominantly double that of Domiz 2 camp. Figure 3 shows the volume of wastewater received at
212 the Fayda WSPs from January 2020 to May 2022.

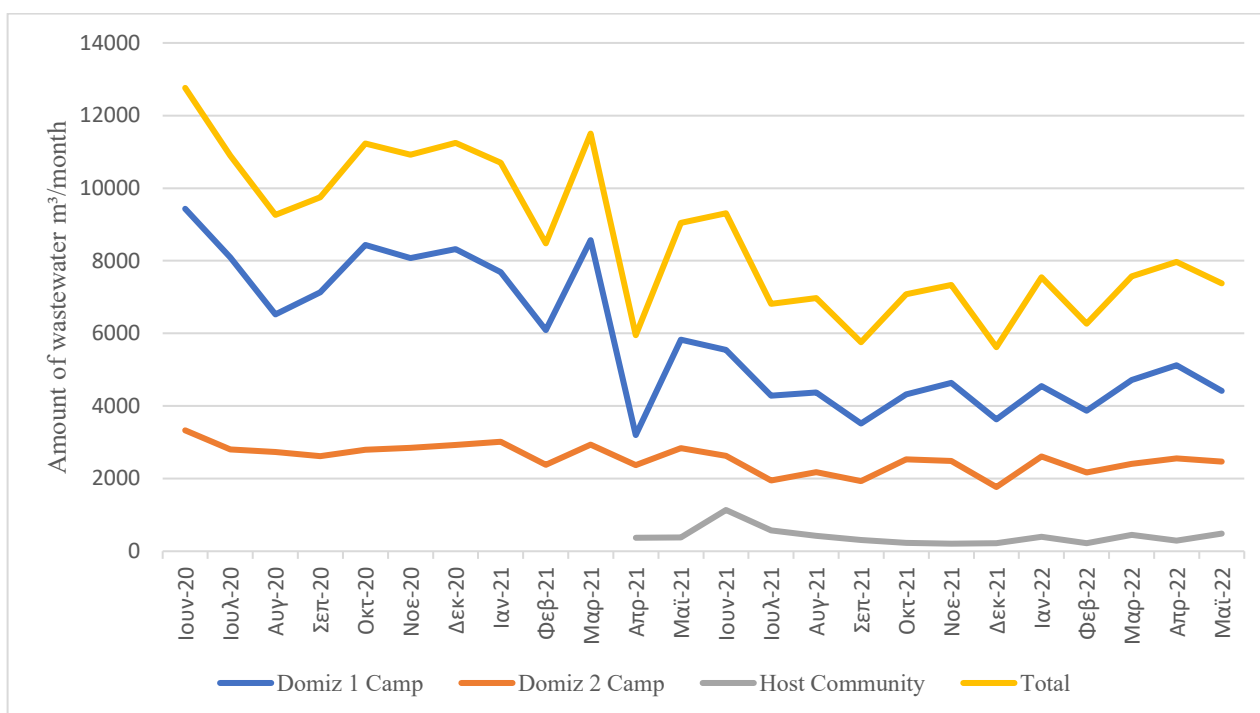
213 Significant variations in wastewater inflow were observed over the course of a 24-month period,
214 indicating possible fluctuations in water consumption patterns, climatic factors, or other potential
215 challenges faced by Fayda WSPs during operation. In April 2021, there was a significant decline in
216 wastewater intake due to the changeover of operations from UNICEF to the contracting business which
217 led to a temporary suspension and a reduction in capacity.

218 The minimum wastewater inflow was recorded in December 2021, reaching a value of 5,620
219 m³/month. This may result from factors such as decreased water usage in the winter months and
220 insufficient money to facilitate the transportation of wastewater from the camps to the treatment plant.

221 The peak wastewater inflow was recorded in June 2020, a value of 12,762 m³/month. This may be
222 related to the availability of money and trucks to assist the transportation of wastewater from the
223 camps to the plant. The average wastewater inflow for the 24 months is 8,640 m³/month which is
224 below the design capacity of the Fayda WSPs for one line which is about 15,000 m³/month.

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Figure 3. Monthly wastewater volumes received at Fayda WSPs from Domiz 1 camp, Domiz 2 camp, host communities, and total inflow during the monitoring period.

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3.1.1 Design vs operational quantities

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The data in Table 1 show the comparison between the quantities that were considered for the design (provided by Directorate General of Municipalities of Duhok (DGoMsD) and the Environment Office of Duhok (EoD)) of the *WSPs* and the current receiving quantities from different locations that were collected during the research months on the vacuum trucks arriving at the treatment plant.

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The present receiving quantities are much lower than the design quantities at the majority of places, particularly in Khanek camp, Fayda sub-district, Sharia sub-district, and Duhok City. This shows that the Fayda WSPs are functioning below their capacity and efficiency and that the collection and

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transportation system of the wastewater from these sites has to be improved. The sites with very low or

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no present receiving quantities are Khanek camp, Fayda sub-district, Sharia sub-district, and Duhok

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City. Increasing the present receiving amounts from these sites will not only improve the performance of the WSPs but also offer environmental and socio-economic advantages for the communities. The observed variability in wastewater inflow is important because changes in hydraulic loading directly influence pond retention time, pollutant dilution, organic loading, and the stability of biological treatment processes.

Table 1. Comparison between design and current wastewater-receiving quantities by source.

#	Locations	Design quantity (trips/day)	Current received quantity (trips/day)
1	Domiz 1	48	16 – 30
2	Domiz 2	22	10 – 16
3	Khanek camp	16	0
4	Fayda Sub-district (Fayda and Domiz)	17	0-2
5	Sharia Sub-district	4	0-1
6	Duhok City (Urban zone)	17	0-2
7	Semel	0	0 – 1
8	Kabarto camp	0	0 – 1

246

247 3.2 *Quality of influent and effluent*

248 Following the assessment of influent quantity, wastewater quality was evaluated to determine how
 249 changes in organic matter, suspended solids, nutrients, pH, and temperature affected the treatment
 250 performance of the Fayda WSPs. Table S1 for the WSP (supplementary material) presents the primary
 251 findings for the water quality parameters (COD, BOD₅, TSS, TN, TP, pH, and Temperature).

252 3.2.1 Chemical Oxygen Demand

253 The influent COD mass balance fluctuates significantly from 693 mg/L to 4022 mg/L which may
254 reflect the variations in the wastewater characteristics and flow rate entering the WSPs plant.

255 Figure 4(a) shows the influent COD mass balance and the effluent COD (from the B4 outlet, the
256 maturation pond) concentrations in different periods of the year. The effluent COD values from May
257 2021 to August 2021 were higher than those from September 2021 to May 2022. While the lowest
258 effluent COD value was documented in May 2021 at 372 mg/L, the highest effluent COD value was
259 reported in May 2021 at 926 mg/L. Considerable variance in effluent COD values was observed
260 throughout different months. This may result from multiple sources, including seasonal variations,
261 changes in influent quality, and operational challenges. The effluent COD concentration ranges from
262 401 mg/L to 926 mg/L.

263 COD removal efficiency was calculated as

264
$$\text{COD removal efficiency} = ((\text{Influent COD} - \text{Effluent COD}) / \text{Influent COD}) * 100 \dots\dots(\text{eq. 1})$$

265 Figure 4(b) depicts the percentage removal of COD for the various times of the year. The average
266 removal efficiency of COD for the entire period was 67.88% for the WSPs plant. The amounts of COD
267 removed from wastewater by the WSP plant differ significantly from one month to another, ranging
268 from 42.1% to 89.3%, indicating variability in the treatment efficiencies of the WSP facility. The
269 minimum removal of 42.1% reflects unstable influent characteristics and operational loading. The
270 removal rate was higher in September (89.3%) and November (84.4%) and lower in July (55.5%) and
271 October (42.1%). This may be related to higher influent COD in September and November compared
272 with July and October. Additionally, it may also be related to the effects of temperature and solar
273 radiation on the rate of biological and photolytic degradation of organic matter in WSPs (Achag et al.
274 2021).

275 Linge et al. (2021) studied the removal efficiency of micropollutants for different WSP configurations
276 at a wastewater oxidation ditch treatment plant. The COD effluent concentration of 28-64 mg/l and
277 average removal efficiency of 88-95% was reported by the authors. WSPs in the tropics with an
278 effluent COD of 100 mg/L and a removal efficiency of 80% were studied by Ho and Goethals (2020).
279 Despite the high removal efficiency, Gerson et al. (2025) specified that the final effluent COD of the
280 Kalobe WSPs in Tanzania was still above the national discharge standard. This means that a high
281 removal efficiency does not automatically translate into effluent compliance when the influent loads
282 are high or variable. Similarly, Akdim et al. (2025) indicated that the Moroccan evaluation of seven
283 WSP systems showed average COD reductions of ~65-70%. Lower and more variable performance in
284 Fayda can be attributed to variable influent quality, variable truck-delivered wastewater sources,
285 changing organic loading, sludge accumulation, and seasonal operational constraints. Thus, the Fayda
286 results suggest that the primary limitation is not the WSP process, but the instability of influent loading
287 and operational control under local field conditions.

288

289 3.2.2 Total Suspended Solids

290 Figure 5(a) demonstrates the influent and effluent TSS levels changed from month to month. The
291 influent TSS mass balance values ranged from 165.39 to 898.71 mg/L, and the effluent TSS
292 concentration ranged from 45 to 420 mg/L. This shows that the WSP plant is effective in eliminating
293 TSS from wastewater.

294 Figure 5(b) represents the percentage removal of TSS in different months of the year. The percentage
295 removal of TSS ranged from 42.31% to 81.08%. Nwankwo et al. (2019) investigated the kinetics of
296 solids removal in WSPs and their results indicated that TSS removal efficiency ranged between 60 and
297 80% depending on hydraulic retention time. The Fayda results partly fall within this range, but the

298 lower removal values indicate periods of reduced settling performance. This may be related to high
299 influent solids variability, algal biomass in the facultative and maturation ponds, possible hydraulic
300 short-circuiting, and sludge accumulation reducing the effective pond volume. Therefore, TSS
301 performance should be interpreted as a combined indicator of influent variability, pond hydraulics, and
302 biological activity rather than as a simple sedimentation outcome.

303 3.2.3 pH

304 Figure 6 depicts the influent pH and effluent pH values for the WSPs at different times of year. The
305 influent pH values vary from 7.32 to 8.05 and the effluent pH values vary from 7.69 to 8.35. In most
306 cases, results show that the effluent pH values have increased post-treatment.

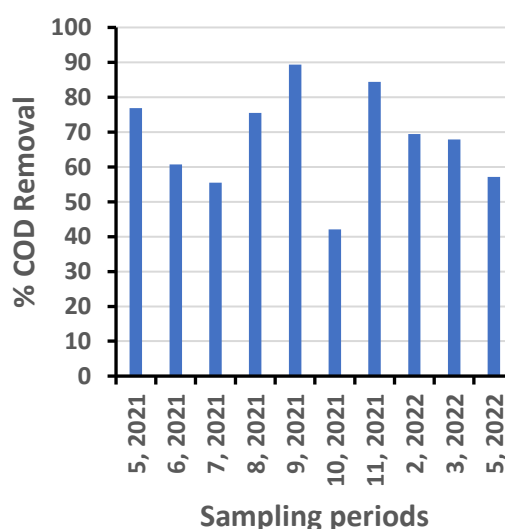
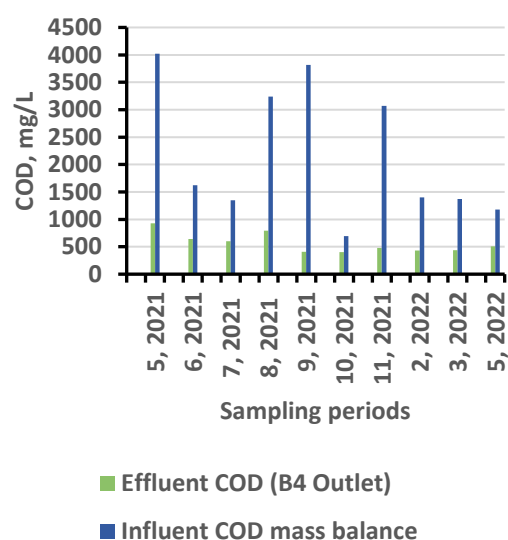
307 According to Kayombo et al. (2005), the influent pH of WSPs ranges from 6.5 to 8.5 depending on the
308 source and composition of wastewater. WSPs have an identified optimal pH range from 7.0 to 8.5 that
309 helps in algal and bacterial growth. Frequent checks on pH values of influent and effluent of WSPs is
310 essential to maintain the efficiency of the treatment processes.

311 3.2.4 Total Nitrogen

312 Figure 7 shows the variation of influent and effluent TN values of the WSPs in different periods of the
313 year. TN covers all forms of nitrogen: ammonia, nitrite, nitrate, and organic nitrogen (Scott 2012).
314 Since the values of the effluent are lower than the values of the influent, this clearly shows that the
315 WSP plant is able to remove nitrogen from the wastewater. The average TN removal efficiency is
316 65%, which is less than the 70% suggested by the World Health Organization (Desye et al. 2022). The
317 influent TN mass balance values ranging between 77.1 and 357.8 mg/L are beyond the normal range of
318 30-100 mg/L for municipal wastewater (Chen et al. 2020). This indicates that the raw wastewater
319 contains a very high nitrogen content, which may in turn affect the efficiency of the WSP plant. The
320 highest value of influent TN mass-balance during October may be linked with a large quantity of

greywater inflow coming from Domiz 1 and Domiz 2 camps. The TN concentration in the effluents varies between 92 and 130 mg/L, and the concentration is above the irrigation limit (Organization 2006). Therefore, the effluents from WSPs require some additional treatment to meet the standards. In the study conducted in Ethiopia, Desye et al. (2022) measured the TN concentrations in both the influent and the effluent of one WSP system. The TN concentration for the influent was between 35.8 and 97.6 mg/L, with the mean being 83.2 mg/L. The TN removal efficiency was 79% which is larger than the 70% target allowed by the World Health Organization (Desye et al. 2022). To compare the results in Figure 7 and the results in the previous study, the WSP facility in Fayda has a larger influent TN concentration than the WSP facility in Ethiopia.

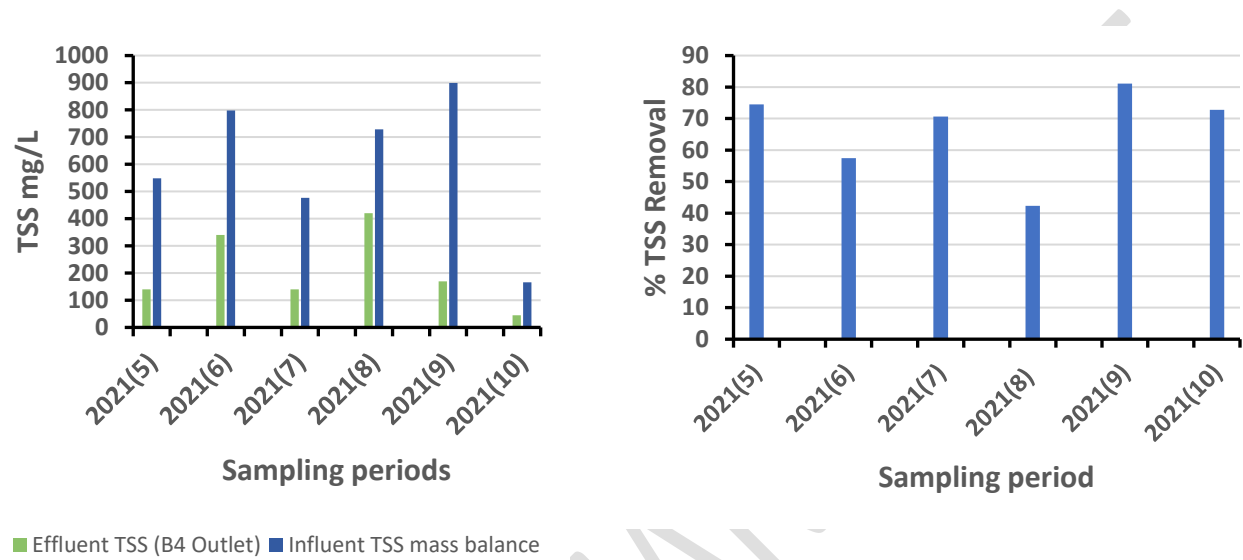
This suggests that the Fayda WSPs were exposed to unusually high nitrogen loading, most likely influenced by greywater inputs from Domiz 1 and Domiz 2 camps. Unlike engineered biological nitrogen-removal systems, conventional WSPs have limited control over nitrification–denitrification pathways. Therefore, the relatively low TN removal in Fayda is consistent with the operational limitations expected for pond systems receiving nutrient-rich and compositionally variable wastewater.



(a)

(b)

Figure 4. Temporal variation of (a) influent and effluent COD concentrations and (b) COD removal efficiency in Fayda WSPs.



(a)

(b)

Figure 5. Temporal variation of (a) influent and effluent TSS concentrations and (b) TSS removal efficiency in Fayda WSPs.

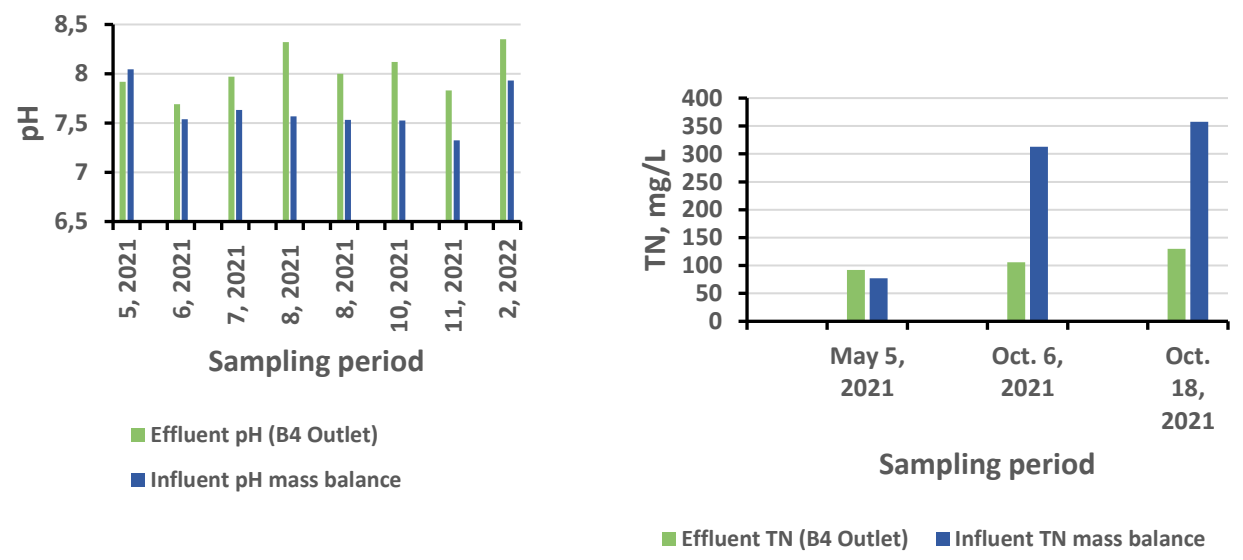


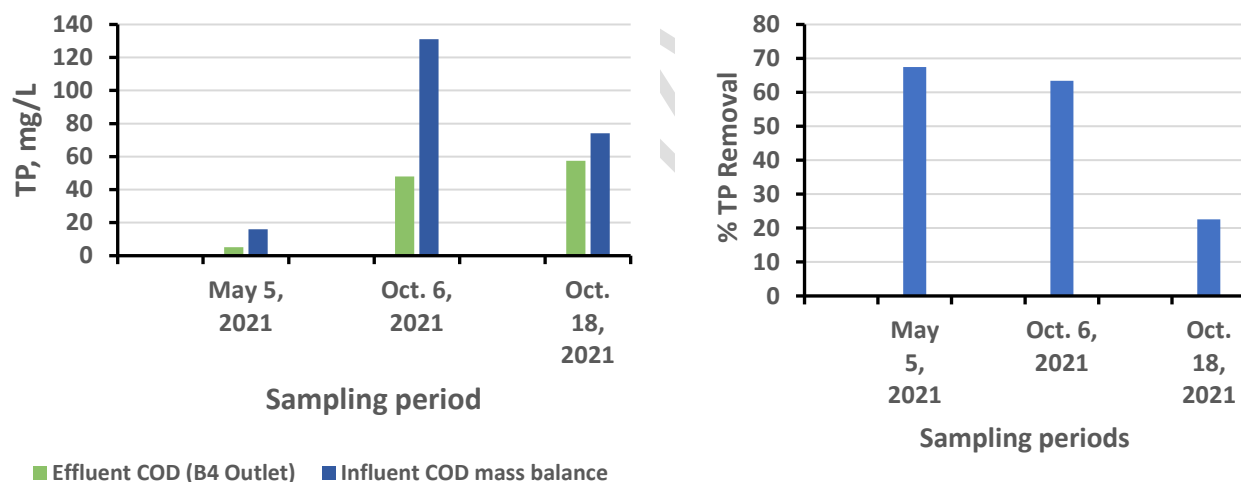
Figure 6. Temporal variation of influent and effluent pH in Fayda WSPs.

Figure 7. Temporal variation of influent and effluent TN concentrations in Fayda WSPs.

3.2.5 Total Phosphorus

TP is a measure of the total phosphorus concentration in the water which comes from different sources such as fertilizers, detergents, organic waste, and industrial effluents. Excess phosphorus in water leads to eutrophication, defined by the overgrowth of algae and aquatic plants depleting dissolved oxygen, therefore negatively affecting water quality and aquatic life. Therefore, it is desirable to remove as much phosphorus as possible from the wastewater before discharging it into the environment (Bunce et al. 2018). According to Figure 8(a), the influent TP concentration in the WSP plant ranged from 16 mg/L to 131 mg/L, while the effluent TP concentration ranged from 5.2 mg/L to 57.4 mg/L. The percentage of TP removed from the influent to the effluent, ranged from 22.6% to 67.5% as shown in Figure 8(b). These results show that the WSP plant was able to reduce the TP concentration in the wastewater, but not consistently or sufficiently. The typical TP removal in WSPs varies from 40% to 80% (Kayombo et al., 2005); however, the studied plant depicted in Figure 8(a) and (b) mostly fell below this range, except on May 5, 2021, when it achieved a removal rate of 67.5%. A case study in Ethiopia (Desye et al. 2022) indicated a 69.2% TP removal. The effluent TP concentration exceeded the permitted discharge limit of 2 mg/L, measuring 5.2 mg/L to 57.4 mg/L. In comparison, the TP removal efficiency in the WSPs facility, illustrated in Figure 8(a) and (b), corresponds with the case study but constantly demonstrates elevated effluent TP concentrations with the exception of May 5, 2021, when it attained 5.2 mg/L. Also, Linge et al. (2021) underlined TP removal variation (32–87%) in WSPs of different configurations and climates. Influenced by biological processes, pond setup, hydraulic regime, and weather conditions, corresponding with the plants' operational capability.

357 Thus, the Fayda values are within the broader range reported in the literature but show weaker
 358 consistency. This is most likely because phosphorus removal in WSPs is dependent on several
 359 processes including algal uptake, sedimentation of particulate phosphorus, adsorption to solids and the
 360 weather conditions as stated by Linge et al. (2021). However, such mechanisms may be unstable under
 361 conditions of sludge accumulation, variable HRT and high greywater-derived phosphorus loading. The
 362 results from the Fayda suggest that additional operational measures such as improved source control,
 363 desludging or post-treatment may be necessary for phosphorus control particularly if the effluent is to
 364 be used for agricultural reuse.
 365



(a)

(b)

Figure 8. Temporal variation of (a) influent and effluent TP concentrations and (b) TP removal efficiency in Fayda WSPs.

3.2.6 Statistical Summaries for Key Parameters

Table 2. Descriptive statistics of the final effluent quality of the Fayda WSPs. Effluent COD values ranged from 372 to 926 mg/L with mean of 550.2 ± 151.3 mg/L and CV of 27.5% indicating

moderate variability. TSS was more variable with a range of 45–420 mg/L, a mean of 189.8 ± 115 mg/L and a CV of 60.6%. The TN was relatively more stable, ranging from 92 to 130 mg/L, with a mean value of 109.33 ± 19.22 mg/L and the lowest CV of 17.6%. TP had the highest variability (CV = 75.5%). Overall the results show unstable effluent quality especially for TSS and TP, requiring improved influent control, and desludging.

Table 2. Descriptive statistics of effluent data for the Fayda WSPs.

Parameter	Effluent range, mg/L	Effluent mean $\pm$ SD	CV (%)
COD	372–926	550.2 ± 151.3	27.5
TSS	45–420	189.8 ± 115	60.6
TN	92–130	109.33 ± 19.22	17.6
TP	5.2–57.4	36.87 ± 27.8	75.5

3.3 Operation and Performance of Fayda WSPs

Water Quality data alone cannot fully explain the variance found in removal rates for COD, TSS, TN, and TP; therefore, the following discussion identifies the factors of operational variables which may affect treatment performance.

Operational variables affecting performance and operation of WSPs include: influent characteristics; HRT; weather; and algae growth. The variation and time of these variables can influence the overall performance of WSPs. (Achag et al. 2021; Von Sperling 2007; Mara 2013). The design of Fayda WSPs was built on an average BOD₅ value for the sewage as considered by the EoD. However, the actual BOD₅ concentrations of the sewage inlet at the Fayda WSPs were higher than the design values, as depicted in Table 3. This factor has an impact on the operation and performance of the ponds and the quality of the treated effluent.

378 **Table 3.** Comparison of design and measured BOD₅ concentrations for wastewater sources.

#	Locations	Average BOD ₅ that considered for the design (mg/L)			Current received average BOD ₅ (mg/L)		
		Mean ± SD	Range (Min-Max)	Coefficient of variation (CV%)	Mean ± SD	Range (Min-Max)	Coefficient of variation (CV%)
1	Domiz 1	566 ± 125	456–703	22.21	1622 ± 1172	775–3658	72.29
2	Domiz 2	411 ± 103	339–529	25.06	811 ± 537	384–1716	66.20
3	Fayda Sub-district	3516 ± 1542	2418–5280	43.88	2993 ± 1989	1587–4400	66.45
4	Duhok City	1370 ± 660	860–2115	48.15	5064 ± 1924	3524–7221	38.00

379

380 The Domiz 1 and Domiz 2 camps, as well as Duhok City, demonstrate higher BOD₅ levels than the

381 design values, indicating an increase in organic loading on the anaerobic ponds. Consequently, the

382 effectiveness of the treatment may be hindered which could lead to odor problems. To improve

383 treatment efficiency, flow rate adjustments are necessary because of the difference between the

384 designed and actual BOD₅ levels. An equalization basin construction before the influent enters the

385 ponds can help mitigate shock loading and stabilize the flow and character of the wastewater. At

386 present, the removal rates of COD and BOD₅ in Fayda WSPs are around 80% and 86%, respectively,

387 representing a good performance for WSPs (Kadri et al. 2021; and Mara 2013). Nevertheless, they are
388 not meeting the design capabilities of the ponds, which could reflect higher effluent concentration than
389 expected.

390 The design was based on values that assumed a certain amount of black wastewater. However, the
391 current influent wastewater contains a high percentage of greywater that comes from Domiz 1 and
392 Domiz 2 camps which have different characteristics than black waste. Greywater typically has higher
393 levels of nitrogen and phosphorus due to detergent and other household chemicals. These nutrients can
394 promote algal growth in the ponds, affecting oxygen balance, light penetration, and sedimentation
395 processes. Algae can produce toxins harmful to aquatic life and human health. Additionally, greywater
396 usually has a lower concentration of organic matter when compared to black wastewater, which may
397 reduce the ponds' biodegradation limitations (Khajvand et al. 2022; Awasthi et al. 2024).

398 The HRT of the Fayda WSPs has undergone changes since the design phase, attributed to the variation
399 in the applied flow. The design HRT was determined using the average daily flow anticipated by the
400 EoD which was 1,052 m³/d. Nonetheless, the existing applied flow is below the design flow; therefore,
401 all ponds have longer HRTs. The current HRTs are still within the recommended ranges for each type
402 of pond; however, for the anaerobic pond 1, it is close to the upper limit. Table 4 illustrates the current
403 detention times and during the design together with the criteria. Extended HRTs can provide both
404 beneficial and detrimental effects on the performance of the WSPs. Longer HRTs can increase the
405 interaction duration between wastewater and microorganisms, hence improving the elimination of
406 organic matter and pathogens. However, prolonged HRTs may elevate the danger of odor generation,
407 sludge accumulation, and nutrient leaching from anaerobic ponds. Extended HRTs might diminish the
408 hydraulic efficiency of ponds which could cause dead zones and short-circuiting (Achag et al. 2021;
409 Von Sperling 2007).

411 **Table 4.** Design and current HRT of Fayda WSP units.
 412

#	Ponds	Designed HRT (days)	Current HRT (days)	Recommended Design Criteria (days) (Kayombo et al., 2005)
1	Anaerobic pond 1	3.22	5.57	1-7
2	Anaerobic pond 2	1	1.62	1-7
3	Facultative pond	9.04	15.5	5-30
4	Maturation pond	3	5.7	Min. 3

413 To enhance the performance of the Fayda WSPs, control methods on the loading of the anaerobic and
 414 facultative ponds are advised. This can be accomplished by increasing the fleet of trucks used to
 415 collect black wastewater from the host communities, as this type of wastewater bears higher organic
 416 content. Additionally, the control can involve manipulating the wastewater flow through either one
 417 series of ponds or both series. Through these control measures, the effluent COD values can be
 418 reduced to values < 500 mg/L, which meet the standards for irrigation (Mizzouri et al. 2017;
 419 Organization 2006).

420 The weather conditions of the Fayda WSPs can significantly affect the operation and performance of
 421 the ponds, specifically temperature and solar radiation. The degree of temperature change has a big
 422 impact on microbial metabolic rates, gas solubility, and water density. Meanwhile, solar radiation
 423 impacts the warming of water, the disinfection of pathogens, and photosynthesis in algae (Achag et al.
 424 2021; Mwamlima et al. 2025). Fayda WSPs, located in hot summer and cold winter regions,
 425 experience changes in performance and in temperature and solar radiation. Summer time experiences
 426 an increase in performance, and, on the contrary, winter experiences a decrease.

427 Another problem that could influence the operation and performance of the Fayda WSPs significantly
428 is the algae growth, particularly in the facultative ponds. These microorganisms use sunlight to create
429 oxygen and biomass. Algae can be beneficial because they are important for the aerobic degradation of
430 organic material by providing oxygen and they can also eliminate certain nutrients and pathogens in
431 the wastewater. However, algae have negative impacts too. Algae utilize oxygen at night when
432 photosynthesis stops, and their decomposition can further increase oxygen demand. In addition, algae
433 may reduce the amount of light that penetrates the water, therefore decreasing the rate of
434 photosynthesis and the rate of disinfecting the water. They can also lead to problems including
435 turbidity, color, and odor in the effluent (Kadri et al. 2021; Sinn et al. 2022). The growth of algae in
436 the Fayda WSPs is affected by several factors, such as nutrient concentrations, HRT, temperature, and
437 solar radiation.

438 The effluent quality of the Fayda WSPs does not meet the criteria for direct discharge to water
439 resources or reuse in irrigation, an interpretation of the Iraqi standards for the use of treated wastewater
440 in irrigation (e.g., BOD<40 mg/L, COD<100 mg/L) (Shakir et al. 2017; Iraqi Facts 2012).

441 This emphasizes the need for clear, enforceable standards for all pathways of discharge. Although the
442 physicochemical results suggest that the final effluent did not always meet discharge or irrigation-reuse
443 standards, the lack of microbiological data is another limitation. In addition to COD, BOD₅, TSS,
444 nutrients and pH limits, monitoring of pathogen indicators is required to confirm safe reuse in the
445 context of wastewater reuse. Kamel et al. (2026) reported variable bacterial and viral decreases in full-
446 scale WSPs and emphasized the need for improved monitoring and management approaches to protect
447 public health.

448

449

450

451 ***3.4 Main Operational Problems and Recommended Improvement Framework***

452 The major constraints on the Fayda WSPs have been classified into six distinct areas based on the
453 operational experiences and performance evaluation as well as the monitoring data from March 2021
454 to May 2022. They include: variability in loading, nutrient enrichment of the effluent, sludge
455 accumulation, improper disposal of effluent, snow-melting drainage and limitations of the existing
456 infrastructure; all of which have an effect on the operation of the wastewater treatment facilities to
457 varying degrees. The list of potential challenges or problems for the Fayda WSPs include:

458 Seasonal loading control should be adopted as a routine operational strategy. During cold periods and
459 snowfall events, biological degradation slows because microbial activity is reduced. Therefore, the
460 organic loading to each pond series should be reduced during winter, while loading may be increased
461 gradually during warmer periods when biological treatment is more active. This can be done by
462 controlling the number of wastewater trucks discharged per day, distributing the flow between Series
463 A and Series B, and avoiding sudden loading changes during low temperature periods. This strategy
464 will reduce odor formation, improve the stability of COD and BOD removal and reduce the risk of
465 effluent deterioration in winter.

466 In the Fayda WSPs, anaerobic and facultative ponds are subject to overload because of different
467 hydraulic loading and the influent BOD and COD concentrations are high. The consequence of this is
468 the establishment of odor, sludge, and nutrient problems together with a drop in the removal efficiency.
469 One of the main improvements is the construction of an upstream equalization basin before the inflow
470 of the wastewater in the anaerobic ponds. This basin would help regulate flow variations, reduce
471 hydraulic shock loading, and homogenize influent wastewater quality before treatment. Such an
472 intervention is especially important as the Fayda WSPs serve wastewater from different sources
473 including Domiz 1, Domiz 2, host communities and other surrounding areas with highly variable

474 influent characteristics. The equalization basin would stabilize the influent flow and pollutant
475 concentration and would reduce sudden changes in BOD, COD, TSS, TN and TP loading and would
476 improve the biological stability of the anaerobic and facultative ponds. However, it should be noted
477 that this solution requires constant average flow pumping.

478 High nitrogen levels in both the influent and effluent are a sign that the removal of nutrients was not
479 efficient and there is a significant risk of eutrophication.

480 Greywater-source management should be considered a high-priority intervention because elevated TN
481 and TP concentrations were strongly associated with wastewater contributions from Domiz 1 and
482 Domiz 2 camps. Greywater may contain detergents, nutrients, and household chemicals that increase
483 nitrogen and phosphorus loads and promote excessive algal growth in facultative ponds. Therefore,
484 source separation of greywater and black wastewater should be investigated in the camps. If full
485 separation is not immediately feasible, practical alternatives include reducing detergent discharge, and
486 improving awareness among camp residents. This intervention would decrease nutrient enrichment,
487 algal overgrowth, turbidity and the risk of eutrophication.

488 The high level of sludge in the anaerobic ponds suggests a considerable organic load coupled with
489 insufficient sludge removal. The level of sludge was measured using the white towel method, the
490 sludge level in the anaerobic A1 pond was 90 cm and in the anaerobic B1 pond was 85 cm. High
491 sludge accumulation can reduce the effective volume and HRT of the ponds and can also cause odor,
492 nutrient, and pathogen problems (Von Sperling 2007). The solution is to remove the excess sludge
493 from the ponds by desludging them when they are one-third full of sludge (by volume). It is important
494 to note that timely desludging will soon be necessary to prevent further complications associated with
495 the high sludge accumulation.

496 Wastewater should not be discharged directly from the facility to a pond without first going through
497 the Intake and Grit Chamber. Bypassing the preliminary treatment process increases the amount of
498 solids and grit, as well as damaging the geomembrane, and reduces pond performance.

499 To prevent this, clear discharge routes should be marked, truck drivers should receive training, and
500 physical barriers should be installed to prevent direct dumping into the ponds. In addition, plant
501 operators should maintain a daily log of truck arrivals, and discharge locations. This low-cost
502 operational measure would improve influent control and protect the physical integrity of the pond
503 system.

504 The excessive application of herbicides along pond embankments can have negative impacts on the
505 organisms living there. Herbicides can leach into ponds, thus compromising water quality as well as
506 the treatment process. The presence of herbicides usually exerts a toxic and nutrient-rich composition
507 and a negative impact on microorganisms and algae, which are the main causes of their harmful effects
508 on ponds. As a result, the efficiency of the pond system is reduced. To resolve this problem, it is
509 essential to minimize the reliance on herbicides and explore alternative strategies for controlling
510 excessive vegetation. These other ways include manual weeding, mowing, or grazing.

511 Snowmelt and stormwater should be diverted away from the treatment ponds because they increase
512 hydraulic loading, dilute wastewater, and inhibits biodegradation processes. The construction of
513 manholes equipped with gate valves between the drying beds and ponds would allow operators to
514 control snowmelt flow during winter. Additionally, a runoff diversion channel should also be
515 constructed to prevent clean runoff from flowing into Anaerobic Pond B1 and redirect this flow to the
516 nearby valley. This practice will reduce hydraulic disturbance of Anaerobic Pond B1 and create a more
517 stable treatment environment for Anaerobic Pond B1 during winter and early spring.

518 The following recommendations are therefore directly linked to the measured performance limitations
519 and are intended to improve treatment stability, effluent quality, operational safety, and the feasibility
520 of controlled wastewater reuse:

521 1. It is necessary to make the Iraqi regulations and criteria for treated wastewater use in irrigation more
522 in compliance with the World Health Organization (WHO) regional standards for wastewater reuse in
523 the Eastern Mediterranean Region. It would also be reasonable to propose specific effluent standards

524 that are more achievable on the basis of categories instead of a single effluent number. It is also
525 necessary that any discharge from the Fayda WSPs intended for irrigation comply with the Jordanian
526 Standard (JS: 893/2002) Column C regarding effluent reuse for irrigation for agricultural crops,
527 industrial crops, and forestry (see Table 5).

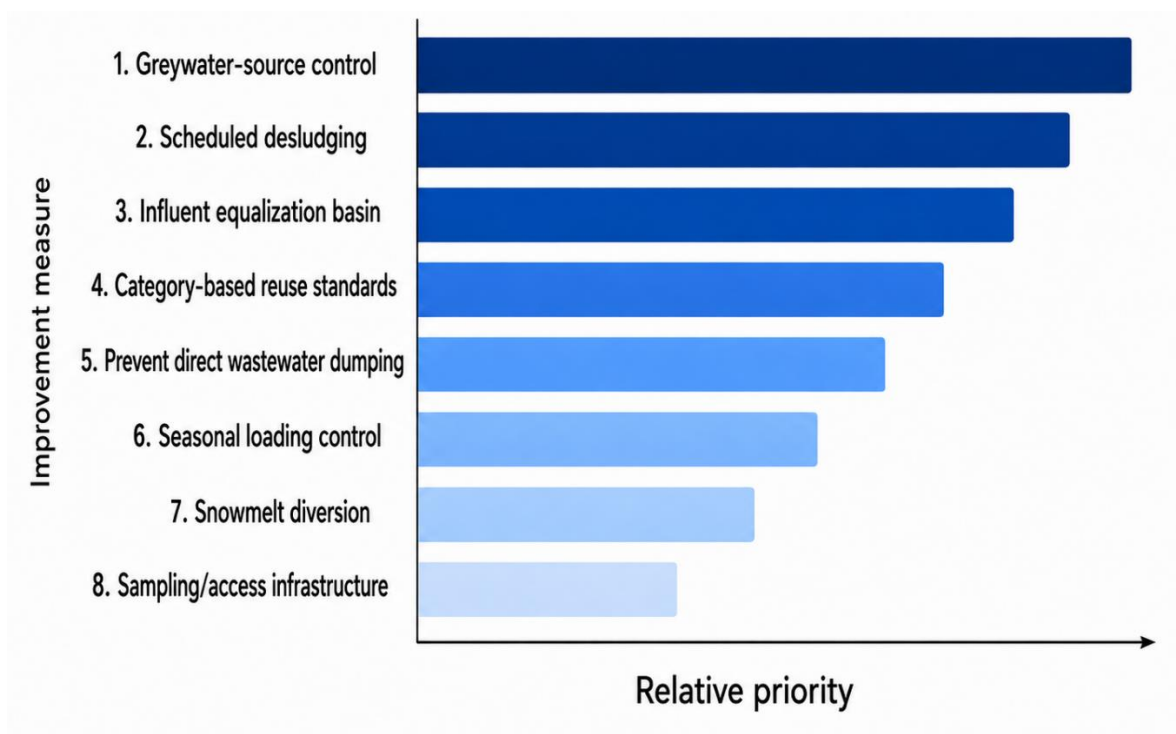
528 2. Improve infrastructure to facilitate sample collection, sludge depth measurements and pond
529 maintenance. For example, Bridge, safe egress, boats and grit chambers.

530

531 3. Increase the design volume and retention time by desludging of the first anaerobic pond. Raising the
532 awareness of the farmers on the benefits of using the sludge as fertilizer.

533 4. Support community financing of sanitation projects including operation and maintenance of Fayda
534 WSPs.

535 5. Introduce routine microbiological monitoring of the final effluent for fecal coliforms, E.coli and
536 intestinal helminth eggs prior to approval for any direct agricultural reuse.



537

538 **Figure 9. Prioritized improvement measures for Fayda WSPs based on observed operational**
 539 **problems, expected treatment benefit, and implementation urgency.**

540 **Table 5.** Comparison of Jordanian wastewater reuse categories with Iraqi standards for treated
 541 wastewater reuse in irrigation.

Parameter	Unit	Cooked	Plenteous	Field	Iraqi standards
		vegetables,	trees and	crops,	for the use of
		parking areas,	green areas,	industrial	treated
		playground and	side of roads	crops and	wastewater in
		side of roads	outside cities	forestry	irrigation (Shakir
		inside cities			et al. 2017; Iraqi
					Facts 2012)
Group		A	B	C	

BOD ₅	mg/L	30	200	300	40
COD	mg/L	100	500	500	100
TDS	mg/L	1500	1500	1500	2500
TSS	mg/L	50	200	300	40
pH	unit	6.0-9.0	6.0-9.0	6.0-9.0	4-8.6
Phosphate (PO ₄)	mg/L	30	30	30	25
Chloride	mg/L	400	400	400	Not specified
Total Nitrogen	mg/L	45	70	100	Not specified
Nitrates	mg/L	30	45	70	50
Sodium	mg/L	230	230	230	250
Calcium	mg/L	230	230	230	450
Magnesium	mg/L	100	100	100	80
SAR	-	9	9	9	6-9
<i>E.coli</i>	MPN/100 mL	100	1000	Not specified	1000
Intestinal helminth eggs	egg/L	≤1.0	≤1.0	≤1.0	Not specified

542

543 4. Conclusion

544 The present study is a full-scale performance evaluation of the Fayda WSPs in Duhok, Iraq, based on
545 16 grab-sampling campaigns and 69 wastewater samples from influent sources, pond outlets and final
546 effluent points. The results demonstrated significant variation in the performance of the treatment.
547 COD removal ranged between 42.1% and 89.3% while the final effluent COD concentrations were
548 high between 401 to 926 mg/L. TSS removal was between 42.31% and 81.08% indicating a moderate

549 but inconsistent solids removal. Average TN removal was about 65% and TP removal ranged from
550 22.6 to 67.5%, so nutrient removal was also limited. The final effluent TN concentrations were in the
551 range of 92 to 130 mg/L and TP concentrations were in the range of 5.2 to 57.4 mg/L, indicating that
552 the treated effluent did not always meet the requirements for direct discharge or for agricultural reuse.

553 The operational assessment revealed that the system was operating below its design hydraulic capacity
554 with an average wastewater inflow of about 8,640 m³/month against a estimated one-line design
555 capacity of about 15,000 m³/month. Therefore, the HRT values in the present situation were higher
556 than the original design values, reaching 5.57 days in Anaerobic Pond 1, 1.62 days in Anaerobic Pond
557 2, 15.5 days in the facultative pond, and 5.7 days in the maturation pond. Sludge accumulation was
558 also considerable as the measured sludge depths were 90 cm and 85 cm in Anaerobic Ponds A1, and
559 B1 respectively. These results confirm that the performance of the treatment was largely limited by
560 fluctuating influent quality, high organic and nutrient loading, greywater inputs, seasonal temperature
561 effects, sludge accumulation and operational limitations.

562 Results indicate that influent equalization, improved loading control, regular desludging, better control
563 of greywater inputs and improved site infrastructure are required to enhance system stability. The
564 study also supports the development of a category-based wastewater reuse framework in Iraq, because
565 a single discharge limit does not adequately reflect the variable performance and potential reuse
566 applications of WSP effluents. The study also acknowledges the important limitation of not including
567 microbiological indicators in the performance assessment. Future studies should include
568 microbiological monitoring, especially fecal coliforms, *E. coli*, and helminth eggs, to provide a more
569 complete assessment of public-health risks associated with wastewater reuse. The main novelty of this
570 study is its integration of field-based performance monitoring, operational diagnosis, and regulatory
571 evaluation for a full-scale WSP system in a refugee-camp and host-community context, providing

572 practical evidence for improving WSP management and wastewater reuse policy in Iraq and similar
573 water-scarce developing regions.

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584

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742 Table S1: Supplementary material ,raw data for the wastewater analysis.

Sample No.	Date	Test	Locations (sources for inlet)		WWTP Ponds outlets			
1	5/5/2021			Domiz 1	Domiz 2	B1 Outlet	B4 Outlet	
		COD (mg/l)		4590	2750	1247	926	
		TSS (mg/l)		529	440	260	140	
		pH		8.18	7.8	7.84	7.92	
		Temp °C		25.8	26.3	26.4	26.1	
		TN (mg/l)		68.5	94.8	74.4	92	
		TP (mg/l)		20	7.8	5	5.2	
		SO4		160	191	143	43.3	
2	16/05/2021	Fayda		Domiz 1	Domiz 2	B1	B2 Outlet	B4
		BOD	4400	1076	599	480	506	410
		COD (mg/l)	11905	1350	960	1011	712	537
		TSS (mg/l)	6485	650	528	320	316	108
		pH	6.93	7.7	7.6	7.47	7.37	7.74
		Temp °C	26.2	28.3	27.6	26.6	26.1	25.6
3	24/05/2021	Duhok		Domiz 1	Domiz 2	B1	B2	B4
		COD (mg/l)	16600	1960	1394	1820	1394	372
		TSS (mg/l)	4561	900	420	690	410	260
		pH	7.8	7.44	7.34	7.41	7.8	7.81
		Temp °C	24	24	24.2	24.3	24.1	24

4	30/05/2021		Duhok		Domiz 1	Domiz 2	B1	B2	B4	
		COD (mg/l)	10221		972	783	696	612	551	
		TSS (mg/l)	3583		452	285	260	235	130	
		pH	7.77		7.61	7.38	7.44	7.68	7.87	
		Temp °C	28.3		28	27	28.2	27.6	26.9	
5	3/6/2021		Fayda	Duhok	Domiz	Domiz 1	Domiz 2	B1	B2	B4
		BOD (mg/l)	1587	3530	3191			274	238	207
		COD (mg/l)	4080	8100	12400	1103	942	734	651	639
		TSS (mg/l)	1500	6240	5020	452	285	260	170	340
		pH	7.34	7.54	7.6	7.61	7.38	7.7	8	7.69
		Temp °C	24.8	25.2	24.9			24.9	24.6	24.3
6	July 2021	Test	Tanahi		Domiz 1	Domiz 2	B1	B2	B4	
		COD (mg/l)	846		1306	616	696	548	600	
		TSS (mg/l)	140		420	160	360	180	140	
		pH	7.7		7.7	7.5	7.7	7.94	7.97	
		Temp °C	25.2		24.7	25.2	24.9	24.8	25.2	
7	August 2021		Domiz				B1		B4	
		COD (mg/l)	3430		3812	1860	680		792	
		TSS (mg/l)	920		690	620	241		420	
		pH	7.7		7.6	7.5	7.83		8.32	
		Temp °C	33.6				32.9		31	
8	20/09/2021				Domiz 1	Domiz 2		B2	B4	
		COD (mg/l)			4320	2720		453	410	
		TSS (mg/l)			680	1120		180	170	
		pH			7.6	7.4		7.7	8	

9	Oct-21				Domiz 1	Domiz 2	B1 Outlet	B2 Outlet	B3 Outlet	B4 Outlet	
		COD (mg/l)			10400	857	774	615	659	585	
		TSS (mg/l)			1835	222	380	195	165	145	
		pH			7.7	7.5	7.7	7.94	7.97	8	
		Temp °C			24.7	25.2	24.9	24.8	25.2		
10	6/10/2021				Domiz 1	Domiz 2		B2	B3		
		COD (mg/l)				890	647	601	599	587	
		TSS (mg/l)			680	1120		220	230		
		pH			7.6	8		7.5	8.1		
		Temp °C			26.6	25.9		28	25.7		
		TN (mg/l)			260	410			270	106	
		TP (mg/l)			142	111		125	64.5	48	
11	18/10/2021				Domiz 1	Domiz 2		B2	B3	B4	
		COD (mg/l)			541	699		536	497	401	
		TSS (mg/l)			126	100		130	60	45	
		pH			7.42	7.7		7.83	7.96	8.12	
		Temp °C			27	26.5		26.6	26.8	26.5	
		TN (mg/l)			410	270		180	161	130	
		TP (mg/l)			82	61		80	59.8	57.4	
12	24/11/2021		A2 Outlet	A3 Outlet	A4 Outlet	Domiz 1	Domiz 2	B1 Outlet	B2 Outlet	B3 Outlet	B4 Outlet
		COD (mg/l)				2860	3270	602	515	465	479
		TSS (mg/l)									
		pH				7.22	7.48	7.52	7.6	7.72	7.83

		Temp °C				25.7	25.4	25.6	25.6	25.6	24.9
13	7/1/2022		A2	A3	A4	Domiz 1	Domiz 2	B1	B2	B3	B4
		COD (mg/l)	788	547	533	2000	3260				
14	28/02/2022		A1	A2	A3	Domiz 1	Domiz 2	B1	B2	B3	B4
		COD (mg/l)	948	707	629	1430	969	831	643		429
		TSS (mg/l)									
		pH	7.75	7.9	8.2	8.05	7.75	7.95	8.1		8.35
15	15/03/2022		A1	A2	A3	Domiz 1	Domiz 2	B1	B2	B3	B4
		COD (mg/l)		880	664	1300	757		662		440
16	10/5/2022		A1	A2	A3	Domiz 1	Domiz 2	B1	B2	B3	B4
		COD (mg/l)				830	920		635	540	505

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